## Exact solutions for N steady fingers in a Hele-Shaw cell

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The problem of the displacement of a more viscous fluid by a less viscous one in a Hele-Shaw cell has received considerable attention, both theoretically and experimentally, since the pioneering work by Saffman and Taylor [1]. In particular, the situation when surface tension effects are neglected is rather amenable to mathematical investigation and several exact solutions have been found in this case. For example, a large class of solutions for steady bubbles in a Hele-Shaw cell has been reported previously by the present author [2]. Exact time-dependent solutions in the form of the so-called pole dynamics have also been extensively investigated in the literature [3]. Of particular interest among these time-dependent solutions is a class of solutions [4,5] whose asymptotic interface corresponds to N steadily moving fingers. The physical relevance of multifingers solutions has been discussed recently [6] in connection with the role of surface tension in the dynamics of fingering patterns. Although the long-time behavior of the N-finger solution has been extensively studied [7,8], an explicit solution for these N steady fingers is nonetheless warranted. To present such a calculation is the chief aim of this Brief Report.

The problem of *N* steady fingers moving with a constant speed *U* in a Hele-Shaw channel in the absence of surface tension is formulated as follows. Let  $\mathcal{D}$  denote the region inside the channel occupied by the viscous fluid and  $C_k$  the air-fluid interface corresponding to the *k*th finger [Fig. 1(a)]. The fluid-velocity field  $\mathbf{v}(x, y)$  is given by

$$\mathbf{v} = \boldsymbol{\nabla} \boldsymbol{\phi},\tag{1}$$

where the velocity potential  $\phi(x,y)$  is the solution to the free-boundary problem

$$\nabla^2 \phi = 0 \quad \text{in } \mathcal{D}, \tag{2a}$$

$$\phi = 0, \quad \nabla \phi \cdot \hat{\mathbf{n}} = U \cos \theta \text{ on } \mathcal{C}_k, \quad (2b)$$

$$\nabla \phi \cdot \hat{\mathbf{n}} = 0 \quad \text{at} \quad y = \pm 1,$$
 (2c)

$$\phi \approx Vx \text{ as } x \to \infty.$$
 (2d)

Here  $\hat{\mathbf{n}}$  is the outward unit vector normal to the interface  $C_k$ ,  $\theta$  is the angle between  $\hat{\mathbf{n}}$  and the *x* axis, and *V* is the far-field fluid velocity. (Without loss of generality I shall henceforth set V=1.) Physically, the velocity potential  $\phi$  is identified (up to a negative constant of proportionality) with the fluid-pressure field.

It is most convenient to analyze the problem in a frame (x',y') moving with fingers. If one introduces the complex variable z=x'+iy', the flow can then be described by the complex potential  $W(z) = \phi'(x',y') + i\psi'(x',y')$ , where  $\phi'$  is the velocity potential in the moving frame and  $\psi'$  is the corresponding stream function. From this point onward, I shall, however, drop the prime notation with the understanding that I will be working solely in the frame where the fingers are stationary. The problem given in Eq. (2) can now be restated as follows: The function W(z) must be analytic in the fluid domain  $\mathcal{D}$  and satisfy the boundary conditions

$$W = -Ux + i\psi_k \quad \text{on} \quad \mathcal{C}_k, \quad k = 1, 2, \dots, N, \tag{3}$$

Im 
$$W = \pm (1 - U)$$
 at  $y = \pm 1$ , (4)



FIG. 1. Flow geometry: (a) the *z* plane, (b) the *W* plane, and (c) the  $\zeta$  plane.

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where the  $\psi_k$ 's are real-valued constants and Im W indicates the imaginary part of W. (For a more detailed discussion of these boundary conditions see Ref. [2].) We can thus view W(z) as a conformal mapping from the fluid domain  $\mathcal{D}$  in the z plane to a region in the W plane that consists of an infinite strip of width 2(U-1) with N horizontal slits [Fig. 1(b)].

Next consider the conformal mapping  $z=f(\zeta)$  from the interior of the unit semicircle in the complex  $\zeta$  plane [Fig. 1(c)] to the fluid domain  $\mathcal{D}$  in the *z* plane. For conciseness, but admittedly in an abuse of notation, I shall write  $W(\zeta)$  for  $W(f(\zeta))$ . Thus  $W(\zeta)$  maps conformally the interior of the unit semicircle in the  $\zeta$  plane onto the flow domain in the *W* plane. Such a mapping can be easily constructed and one finds that  $W(\zeta)$  is given by

$$W_{\zeta} = \frac{2(U-1)}{\pi} \frac{\prod_{k=1}^{N} (\zeta - e^{i\gamma_{k}})(\zeta - e^{-i\gamma_{k}})}{\zeta(1 - \zeta^{2})\prod_{k=2}^{N} (\zeta - e^{i\nu_{k}})(\zeta - e^{-i\nu_{k}})}, \quad (5)$$

where the  $\zeta$  subscript denotes derivative with respect to  $\zeta$ . Here  $\gamma_k$  and  $\nu_k$  are real-valued parameters taking values in the range  $0 = \nu_1 < \gamma_1 < \nu_2 < \gamma_2 < \nu_3 < \cdots < \gamma_N < \nu_{N+1} = \pi$ , where for convenience I have also introduced the parameters  $\nu_1 = 0$  and  $\nu_{N+1} = \pi$ . As indicated in Fig. 1, the points  $\zeta$  $= \exp(i\gamma_k)$  and  $\zeta = \exp(i\nu_k)$  are mapped, respectively, on the tips and end points of the fingers.

The mapping function  $f(\zeta)$  can now be obtained by first noting that on  $|\zeta| = 1$  we have  $x = \frac{1}{2}(z + \overline{z}) = \frac{1}{2}[f(\zeta) + f(1/\zeta)]$ . Inserting this identity into the condition (3) yields the equality

$$f(\zeta) + f(1/\zeta) = -\frac{2}{U}W(\zeta),$$
 (6)

which is valid on  $|\zeta| = 1$  and, by analytic continuation, inside the unit semicircle as well. Using the fact that  $W(1/\zeta) = W(\zeta)$ , one can then easily verify that the solution to Eq. (6) is given by

$$f(\zeta) = -\frac{1}{U} \left[ \frac{2}{\pi} \ln \zeta + W(\zeta) \right]. \tag{7}$$

Integrating Eq. (5) to yield  $W(\zeta)$  and inserting this into Eq. (7), one finally obtains

$$f(\zeta) = -\frac{2}{\pi} \ln \zeta + \frac{2}{\pi} (1 - U^{-1}) \bigg[ a_1 \ln(1 - \zeta) + a_{N+1} \ln(1 + \zeta) + \sum_{k=2}^{N} a_k \ln(\zeta - e^{i\nu_k}) (\zeta - e^{-i\nu_k}) \bigg].$$
(8)

Here the coefficients  $a_k$ , in terms of the original parameters  $\gamma_k$  and  $\nu_k$ , are given by

$$\prod_{l=1}^{N} (\cos \nu_k - \cos \gamma_l)$$

$$a_k = \frac{\prod_{l=1}^{l=1}}{\prod_{\substack{l=2\\l\neq k}} (\cos \nu_k - \cos \nu_l)}$$
(9)

for k = 1, ..., N+1. The interface shape for each of the N fingers is then obtained from the parametric equations

$$x_k(\theta) + iy_k(\theta) = f(e^{i\theta}), \quad \nu_k < \theta < \nu_{k+1}, \quad k = 1, \dots, N.$$
(10)

Equations (8)–(10) thus give a 2*N*-parameter (corresponding to *N* parameters  $\gamma_k$ , *N*–1 parameters  $\nu_k$ , and the speed *U*) family of solutions for *N* steady fingers in a Hele-Shaw channel in the absence of surface tension. Note that for a given set of parameters { $\gamma_k$ ,  $\nu_k$ } solutions for arbitrary velocity *U*>1 are possible. (This is the characteristic degeneracy of Hele-Shaw flows without surface tension [1].) Here, however, we need to concern ourselves only with the solutions for *U*=2. Solutions for any value *U*>1 can be obtained from a mere rescaling of the *U*=2 solutions, as shown in Ref. [2]. More precisely, if  $(\hat{x}_k(\theta), \hat{y}_k(\theta))$  denotes a particular solution with *U*=2, then there will exist a corresponding solution for an arbitrary *U*>1 whose parametric equations are [2]

$$x_k(\theta) = (1+\mu)\hat{x}_k(\theta), \qquad (11)$$

$$y_k(\theta) = (1 - \mu)\hat{y}_k(\theta), \qquad (12)$$

where  $\mu = 1 - 2U^{-1}$ .

Setting U=2 in Eq. (8) and evaluating  $f(e^{i\theta})$ , one obtains after some simplification that the interface corresponding to the *k*th finger has the equation

$$x_{k} = \frac{a_{1}}{\pi} \ln \sin \frac{\pi}{2} (y_{k}^{0} - y) + \frac{a_{N+1}}{\pi} \ln \cos \frac{\pi}{2} (y_{k}^{0} - y) + \frac{1}{\pi} \sum_{l=2}^{N} a_{l} \ln [\cos \pi (y_{k}^{0} - y) - \cos \nu_{l}], \quad (13)$$

where

$$y_k^0 = 1 - \frac{a_1}{2} - \sum_{l=2}^k |a_l|, \qquad (14)$$

and the variable y (over the *k*th finger) is restricted to the interval

$$\frac{\nu_k}{\pi} < y_k^0 - y < \frac{\nu_{k+1}}{\pi}, \quad k = 1, \dots, N.$$
 (15)

In Eq. (13) an additive constant has been removed by appropriately redefining the origin of the *x* axis.

A geometrical interpretation of the solution parameters is now straightforward. From Eq. (15) it immediately follows that the relative width  $\lambda_k$  of the *k*th finger with respect to the channel width is given by

$$\lambda_k = \frac{1}{2\pi} (\nu_{k+1} - \nu_k), \quad k = 1, \dots, N.$$
 (16)

From Eq. (8) one also readily sees that the coefficients  $a_k$  fix the separation ("gaps") between adjacent fingers. More specifically, the relative gap  $\delta_k$  (with respect to the channel width) between the (k-1)th and *k*th finger is simply

$$\delta_k = \frac{|a_k|}{2}, \quad k = 2, \dots, N. \tag{17}$$

Similarly,  $\delta_1 = \frac{1}{4} a_1$  is the relative separation between the first finger (from top down) and the upper sidewall, whereas  $\delta_{N+1} = \frac{1}{4} a_{N+1}$  is the corresponding gap between the *N*th finger and the lower sidewall. Let us now denote by  $\Lambda = \sum_{k=1}^{N} \lambda_k$  the total relative width of all the fingers combined and by  $\Delta = \sum_{k=1}^{N} \delta_k$  the total portion occupied by the fluid (on the far left side of the channel), so that  $\Lambda + \Delta = 1$ . For a solution with U=2 we must have  $\Lambda = \Delta = 1/2$  which in turn implies that the parameters  $a_k$  must satisfy the additional condition

$$a_1 + a_{N+1} + 2\sum_{k=2}^{N} |a_k| = 2.$$
 (18)

Thus all possible solutions can be conveniently constructed by prescribing the widths of the *N* fingers (which determine the parameters  $\nu_k$ ) together with the gaps between adjacent fingers (which fix the coefficients  $a_k$ ). Shown in Fig. 2 is a solution for N=3 with  $\lambda_1=0.24$ ,  $\lambda_2=0.11$ , and  $\lambda_3=0.15$ .

Finally, I note that the solution for an asymmetrical finger originally obtained by Taylor and Saffman [9] can be recovered from our generic solution (13) by simply setting N = 1. This yields



FIG. 2. Solution for N=3 with  $\nu_2=1.5$ ,  $\nu_3=2.2$ ,  $a_1=0.3$ ,  $a_2=0.2$ , and  $a_3=0.4$ .

$$x = \frac{a_1}{\pi} \ln \cos \frac{\pi}{2} \left( \frac{a_2}{2} - y \right) + \frac{a_2}{\pi} \ln \sin \frac{\pi}{2} \left( \frac{a_2}{2} - y \right), \quad (19)$$

where the parameters  $a_1$  and  $a_2$  must satisfy the condition  $a_1 + a_2 = 2$ . Introducing the asymmetry parameter  $y_0 = \frac{1}{4} (a_2 - a_1)$ , Eq. (19) can then be rewritten as

$$x = \frac{1}{\pi} \ln \cos \pi (y - y_0) + \frac{2y_0}{\pi} \ln \tan \left[ \frac{\pi}{4} + \frac{\pi}{2} (y - y_0) \right],$$
(20)

where an additive constant has been removed so as to conform with the original choice of coordinates by Taylor and Saffman [9]. Equation (20) thus reproduces the original Taylor-Saffman finger [see Eq. (21) in Ref. [9]].

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